APPENDIX 5 DESKTOP GEOTECHNICAL & HYDROGEOLOGICAL ASSESSMENT REPORT





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March 18, 2024

To: Andrew McGregor Senior Planner / Project Manager, EA & Approvals R.V. Anderson Associates Limited 43 Church Street, Suite 104, St. Catharines ON L2R 7E1

From: Frank C. Liu, P.Eng. & Jason Cole, M.Sc., P.Geo.

Re: Desktop Geotechnical and Hydrogeological Assessment for Water Storage Facility Sites Carlisle Well

1. Introduction

Palmer Environmental Consulting Group Inc. (Palmer) was retained by R.V. Anderson Associates Limited (RVA) (the "client") to complete a desktop geotechnical and hydrogeological assessment in support of the proposed Municipal Class Environmental Assessment (EA) and Conceptual Design for the Carlisle Water Storage Facility located in the Town of Carlisle, within the City of Hamilton (the "project" or the "sites") (**Figure 1**).

Based on information from the Client, two (2) potential Water Storage Facility Sites are proposed (**Figure 1**). *Site 1* is Tower Park, located at 42-46 Woodend Drive, Carlisle and *Site 2* is located at 1535 Centre Road, Flamborough.

The purpose of this desktop geotechnical and hydrogeological assessment is to provide a preliminary characterization of regional setting and subsurface conditions for the two sites and to assess the expected soil mechanic properties, assess potential groundwater issues, identify data gaps and to make recommendations for additional, site-specific work, if required.

Based on information from the client and knowledge of the existing water supply system of Carlisle, the proposed storage facility is expected to include:

- Water Storage Building/Structure;
- Access road and vehicle parking; and
- Associated appurtenances, which may include a treatment facility and/or pump house.

It is noted that the Municipal Class Environmental Assessment has not determined the type of storage facility, and both elevated storage tank and underground storage tank are possible options.

2. Methodology and Data Sources

The geotechnical and hydrogeological assessment was conducted through a desktop study based on data available from multiple public sources, and consulting reports provided by the client.

The major source of data for the current study are the well records collected from Ministry of the Environment, Conservation and Parks (MECP) water well dataset (**Figure 1** and **Appendix A**).

Data from other public sources include, but not limited to, Ontario Geological Survey (OGS: physiography, geology and geotechnical boreholes), MECP, municipalities, conservation authorities, and other public agencies. The data was collected, analysed and synthesized to characterize physical and environmental settings of the two proposed sites. The physical and environmental setting will direct site subsurface condition characterization.

3. Summary of Site Soil and Groundwater Conditions

3.1 Stratigraphy

Surficial geology of both Sites was mapped by OGS as Ice-Contact Stratified deposits of gravel and sand, minor till, in the facies of esker, kame, end moraine, ice-marginal delta and subaqueous fan (**Figure 2**). Bedrock under the overburden below both sites was mapped by OGS as Amabel Formation bedrock, which is described a thick-bedded, crinoidal, locally biohermal and locally bituminous dolostone. Solution enhanced fractures and karstic features are known to be present within the Amabel Formation.

Three (3) well records were identified near Site 1 and four (4) well records were identified adjacent to Site 2 (**Appendix A**). Only well record (6807563) had stratigraphic data for Site 1. All of the well records near Site 2 have stratigraphic data, but only well records (6806877 and 6809946) were used for this assessment as they are located closes to the Site. FDC03RR is 700 m east of Site 1. The information from the well log of FDC03RR can be used to predict stratigraphy at Site 1 and Site 2.

Based on the information from the well records identified at the two Sites with reference to information from other sources, the stratigraphy conditions for the two Sites are summarized in **Table 1**. The elevation data was acquired from Conservation Halton and is also shown in **Figure 1**. While expected to be generally accurate, it should be noted that the stratigraphic data from the MECP water well records should be viewed with a degree of uncertainty.

Data	Site 1 (WWR #6807563)	Site 2 (WWR #6806877 & #6809946)
Ground Surface Elevation (masl)	271.0 – 276.0 masl	265.0 – 272.0 masl
Stratigraphic Unit and Depth	Sand and gravel, trace boulders: 0 – 12.7 m	Sand, some gravel: 0 – 18.3 m
Range (m)	Limestone: 12.7 – 38.1 m	Limestone: 18.3 – 26.5 m
	Shale: 38.1 – 39.6+ m	Shale: 26.5 – 30.5+ m

Table 1. Anticipated Stratigraphy for Site 1 and Site 2

3.2 Groundwater

Groundwater information recorded in the well records is related to the groundwater in bedrock supply aquifers. Groundwater table in overburden should be much shallower. Based on observations during drilling the redundant well, FDC03RR, as well as the well log for the sentry well (CM-03-03S/D) located to the east of the two sites (**Appendix A** and **Figure 1**), the groundwater table in the area close to the two Sites should range from 4.0 to 6.0 meters below groundwater surface (mbgs), however a shallower water table may occur seasonally.

3.3 Source Water Protection

The two Sites are situated in the Halton Region Source Protection Area and is subject to the Source Protection Plan of Halton-Hamilton Source Protection Region. The Source Water Protection Plan identifies four main regulatory factors under the *Clean Water Act (2006)* relating to local hydrogeology to consider: Significant Groundwater Recharge Areas (SGRAs), Highly Vulnerable Aquifers (HVAs), and Wellhead Protection Areas (WHPAs), and Intake Protection Zones (IPZs).

A Wellhead Protection Area (WHPA) is the area around the wellhead where land use activities have the potential to affect the quality or quantity of water that flows into the well. These areas are delineated into zones of vulnerability (A, B, C, and D) based on the time of travel of water into the well, and zones around a surface water body influencing a Groundwater Under Direct Influence (GUDI: E, F). Other zones (Q1, and Q2) are defined as the areas where new water takings or reduced recharge could impact the quantity of water available to municipal supply wells. IPZs are the area on water and land surrounding a municipal surface water intake. HVAs are aquifers that are susceptible to contamination as a result of the soil structure/material or due its location near the ground surface. Lastly, SGRAs are areas where recharge is important to maintain the water level in a community drinking water aquifer.

Based on the provincial dataset, Site 1 is located within a WHPA-A with a score of 10 and a SGRA, and the east part of Site 2 is located within a SGRA (**Figure 3**). WHPA-A with a score of 10 indicates that Site 1 is located within 100 m from the existing supply wells, and that surficial contaminants at Site 1 have a higher risk to migrate into the well screen of the nearby supply well(s).

3.4 Natural Heritage

Based on provincial dataset, no natural heritage features were identified within the two Sites. A wetland is identified adjacent to the south boundary of Site 2. The wetland is a not identified as a Provincially Significant Wetland.

The majority of Site 2 is located within the regulation limit for Conservation Halton. Site 1 is outside of the regulation limit for Conservation Halton.

4. Desktop Geotechnical Assessment

4.1 Foundation Considerations

As presented above, the proposed storage facility may include an elevated storage tank or underground storage tank and associated appurtenances. The major lithological units under both Sites are coarse grained sand and gravel underlain by limestone and shale. Based on the structural forms of the proposed development and the site stratigraphy, spreading footings are expected to be feasible for both elevated storage tank and underground storage tank options. The spread footing for the elevated storage tank may take forms of reinforced concrete raft foundation and reinforced concrete ring. The spread footing for the underground storage tank may take forms of reinforced concrete raft. The spread footing for supporting appurtenances may be conventional strip footing.

It should be noted that the spread footings have to be founded in native soil. The depth of fill will be determined through Site-specific borehole drilling completed during later design stages.

Bearing capacity of foundation soil should be determined through borehole drilling and in-situ testing such as Standard Penetration Test (SPT) and soil classification as part of a geotechnical drilling program.

Bearing capacity of foundation soil for appurtenances structures can be determined either with in-situ SPT test and soil classification as part of a geotechnical drilling program, or with in-situ footing soil inspection conducted by Palmer's experienced geotechnical staff during excavation. Footing soil inspection is usually conducted with a steel rod or a penetrometer coupled with soil classification. The experience of the inspector plays a key role in determining the bearing capacity, and the estimated bearing capacity values can only be used to apparently firm foundation soil and appurtenant structures.

Based on information of lithology as recorded in well records within and adjacent to the sites and well logs from the nearby site, for a preliminary foundation design, 70 to 100 KPa bearing capacity of soil under the sites for spread footings can be considered subjected to confirmation by geotechnical inspection that the soil must be native ice-contact deposits and over 1.5 m deep.

The foundation should be founded on firm native mineral soil and with a depth of more than 1.2 m to be below the front line.

In case the thickness of fill is greater than 1.2 m, the fill should be excavated and removed. The space should be backfilled with lean concrete to grade. Lean concrete should be designed to have a compressive strength over 5.0 MPa.

4.2 Frost Penetration and Foundation Depth

The frozen depth at the two sites is prescribed as 1.2 m on the Ontario Provincial Standard Drawing (OPSD 3090.101), which is the same as the minimal foundation depth of 1.2 m provided in Table 9.12.2.2 of the Ontario Building Code (2012). The spread footing depth of 1.2 m or more should be adequate to protect the foundation from frost heave. Based on the above site characterization, the overburden soil is not frost heave or adfreezing prone. Consequently, frost heave and adfreezing should not be a significant issue if the foundation is founded to a depth of 1.2 m or more and backfilled with well drained materials.

4.3 Excavation and Groundwater Control

The majority of excavation will go through sand and gravel. Based on the density of soil and classification as observed during drilling the redundant well, a light to medium duty backhoe excavator should be adequate to execute the excavation.

Excavation sequence, cutting slope forms and support system should be implemented in accordance with Regulation 213/91 under the Ontario Occupational Health and Safety Act (OHSA) and Ontario Building Code. For the purpose of Regulation 213/91, the soil to be excavated at the Site can be classified as Type 3. The following lists the major criteria that a support system is required by the regulation for Type 3 soil:

- Excavation is deeper than 1.2 m below grade;
- Cutting walls are not sloped from its bottom with a slope having a minimum gradient of one vertical to one horizontal; and
- There will be workers working close to cutting walls for all excavation.

As presented above, the excavation may extend to deeper than 1.2 mbgs, and there must be workers working in the trench to build foundation. Therefore, supporting system has to be considered if the cutting slope is not to be flattened to one vertical to one horizontal (1:1 slope or 45 degree natural slope).

Excavation should be closely inspected by qualified geotechnical staff. If soil condition exposed is different from findings from boreholes, excavation process and shoring system might have to be modified.

Excavated soil should be stockpiled at least 3 m away from the cutting wall crest if space is available.

Unsupported excavation sequence should be arranged such as to minimize the time of the exposure of cutting slopes to elements and to execute the excavation in dry season if possible. Tarping may be needed during extended period of rainfall to prevent erosion and soaking of the slope. Care should be taken to direct surface water away from the open excavations.

Excess soil should be disposed of according to Ontario Regulation 406/19 under the Ontario Environmental Protection Act and associated guidelines.

As mentioned above, the groundwater table under the two sites should be deeper than 3.0 m. If the excavation depth does not extend deeper than 3.0 m, groundwater seepage into the excavation pit is not anticipated. However, considering the coarse grain size of the overburden soil, perched groundwater seepage during precipitation is anticipated, which will be discussed below.

In case the groundwater is encountered at shallower depth, construction dewatering will have to be considered. Hydrogeological assessment will be recommended for each site to determine if construction dewatering is needed.

4.4 Consolidation and Settlement

Based on available lithological information of overburden soil, the founding soil and the underlying soil are not anticipated to be compressible. Drainage-consolidation due to structure loading (primary settlement) is not anticipated. Initial and secondary settlement due to soil grain re-arrangement caused by structure loading will be determined with in-situ SPT tests and soil classification as part of a geotechnical drilling program recommended below.

4.5 Seismic Considerations

The 2012 Ontario Building Code (OBC 2012) came into effect on January 1, 2014 and contains updated seismic analysis and design methodology. The seismic site classification methodology outlined in the code is based on subsurface conditions within the upper 30 m below grade.

As shown in Table 4.1.8.4A of the OBC, three methods of determining the site class are provided in the code: method 1 based on average shear wave velocity, method 2 based on average standard penetration resistance (N-value), and method 3 based on undrained shear strength. Because no information and data about the shear wave velocity, N-values and undrained shear strength are available, seismic conditions can not be assessed at this stage.

5. Desktop Hydrogeological Assessment

As presented above, Site 1 is located within a WHPA-A, and Site 1 and part of Site 2 are located in a Significant Groundwater Recharge Area (SGRA). Moreover, both sites are located in Carlisle Well Field, and Site 1 contains existing supply wells.

Groundwater levels are anticipated to be deeper than 3.0 m for both sites. If the excavation does not extend deeper than 3.0 m, construction dewatering for groundwater seepage should be minimal. If no construction dewatering for control of groundwater seepage is required, other related issues such as a Permit To Take Water (PTTW), an Environmental Activity and Sector Registry (EASR), impacts to natural heritage and interference with other water users, and dewatering-induced soil settlement would not be expected to occur.

As presented above, the shallow overburden is composed of ice-contact stratified deposits. The stratified deposits are expected to have high horizontal hydraulic conductivity values (K-values) in the range of 10^{-5} m/s. Therefore, a large quantity of transient groundwater seepage during precipitation events is anticipated. The contractor should have a sump pump with adequate capacity in place if the excavation occurs during the wet season to deal with potential perched, transient groundwater seepage and stormwater accumulation. Depending on the excavation depth and the rate of groundwater ingress, active dewatering methods such as well points or eductors may be required. Any construction dewatering in excess of 50,000 L/day is required to be registered on the MECP EASR system. Any construction dewatering in excess of 400,000 L/day requires a Category 3 PTTW from the MECP.

Based on the above preliminary characterization of site subsurface conditions, the hydrogeological conditions are considered to be suitable for shallow subsurface construction of the proposed storage facility and appurtenances. No significant groundwater constraints were identified through the desktop assessment for either Site 1 or Site 2. A Site-specific hydrogeological field program is recommended during later design



stages to confirm water table depth, soil permeability and our interpretation of the low potential for adverse effects.

The following are recommendations for the prevention of potential contamination caused by construction activities within a WHPA and SGRA:

- Appropriate awareness training of field staff on the vulnerability of the existing supply wells;
- Spill management plan has to be formulated to meet construction requirement and pass the review of the Risk Management Officer (RMO) of the City of Hamilton; and
- The construction area should be fenced and marked with clear signage for protection of existing supply wells; and
- The City's staff should inspect the construction site periodically for the purpose of onsite contamination prevention.

6. Conclusion and Recommendations

This desktop geotechnical and hydrogeological assessment was based on regional data, secondary source data and available MECP water well records within and close to the Sites. Through the desktop study, preliminary physical and environmental settings, as well as site conditions are characterized, and a preliminary assessment of geotechnical and hydrogeological conditions was provided.

The results of the geotechnical and hydrogeological assessment shows that soil mechanical properties and groundwater conditions at both Site 1 and Site 2 are considered generally suitable for the proposed water storage facility and appurtenance structures. Significant geotechnical and hydrogeological constraints are not anticipated. Geotechnically, both Site 1 and Site 2 will be appropriate for the proposed development. Hydrogeologically, Site 1 is moderately preferred to Site 2 as groundwater levels under Site 1 are predicted to be deeper, and the possibility of construction dewatering requirement is lower.

The above assessment and discussion were based on desktop studies only and should be verified or confirmed with further investigations, including Site-specific field investigations. The following is the recommended steps:

- Geotechnical and hydrogeological drilling should be conducted for the site selected. The drilling should extend to dense to very dense soils or bedrock expected at approximately 30 m depth. The drilling program should include at least three (3) boreholes outside but adjacent to the footprint of the storge tank. SPT testing, soil sampling and lab testing and classification should be completed. Groundwater monitoring wells should be installed in all boreholes to measure stabilized groundwater levels;
- At least one borehole for each appurtenance structure should be drilled to a depth of 6 m and completed as a groundwater monitoring well. SPT testing, soil sampling and lab testing and classification should be completed; and

• To facilitate soil management during excavation as required by O.Reg. 406/19, an Assessment of Past Uses (AP) is recommended during later design stages.

7. Closure

We trust that the information contained in this assessment meets your requirements. Should you have any questions, please do not hesitate to contact our office. The report is subject to the statement of limitations provided at the end of the report.

Yours truly,





Prepared By:Frank C. Liu, P. Eng. & P.Geo.Senior Hydrogeologist



Reviewed By:

Jason Cole, M.Sc., P.Geo. VP, Principal Hydrogeologist

Statement of Limitations

The extent of this study was limited to the specific scope of work for which we were retained and that is described in this report. Palmer has assumed that the information provided by the client or any secondary sources of information are factual and accurate. Palmer accepts no responsibility for any deficiency, misstatement or inaccuracy contained in this report as a result of omissions, misinterpretations or negligent acts from relied upon data. Judgment has been used by Palmer in the interpretation of the information provided but subsurface physical and chemical characteristics may differ from regional scale geology mapping and vary between or beyond well/borehole locations given the inherent variability in geological conditions.

Palmer is not a guarantor of the geological or groundwater conditions at the subject site, but warrants only that its work was undertaken and its report prepared in a manner consistent with the level of skill and diligence normally exercised by competent geoscience professionals practicing in the Province of Ontario. Our findings, conclusions and recommendations should be evaluated in light of the limited scope of our work.

The information and opinions expressed in the Report are for the sole benefit of the Client. NO OTHER PARTY MAY USE OR RELY UPON THE REPORT OR ANY PORTION THEREOF WITHOUT PALMER'S WRITTEN CONSENT AND SUCH USE SHALL BE ON SUCH TERMS AND CONDITIONS AS PALMER MAY EXPRESSLY APPROVE. Ownership in and copyright for the contents of the Report belongs to Palmer. Any use which a third party makes of the Report is the sole responsibility of such third party. Palmer accepts no responsibility whatsoever for damages suffered by any third party resulting from use of the Report without Palmer's express written permission. Should the project design change following issuance of the Report, Palmer must be provided the opportunity to review and revise the Report in light of such alteration or variation.

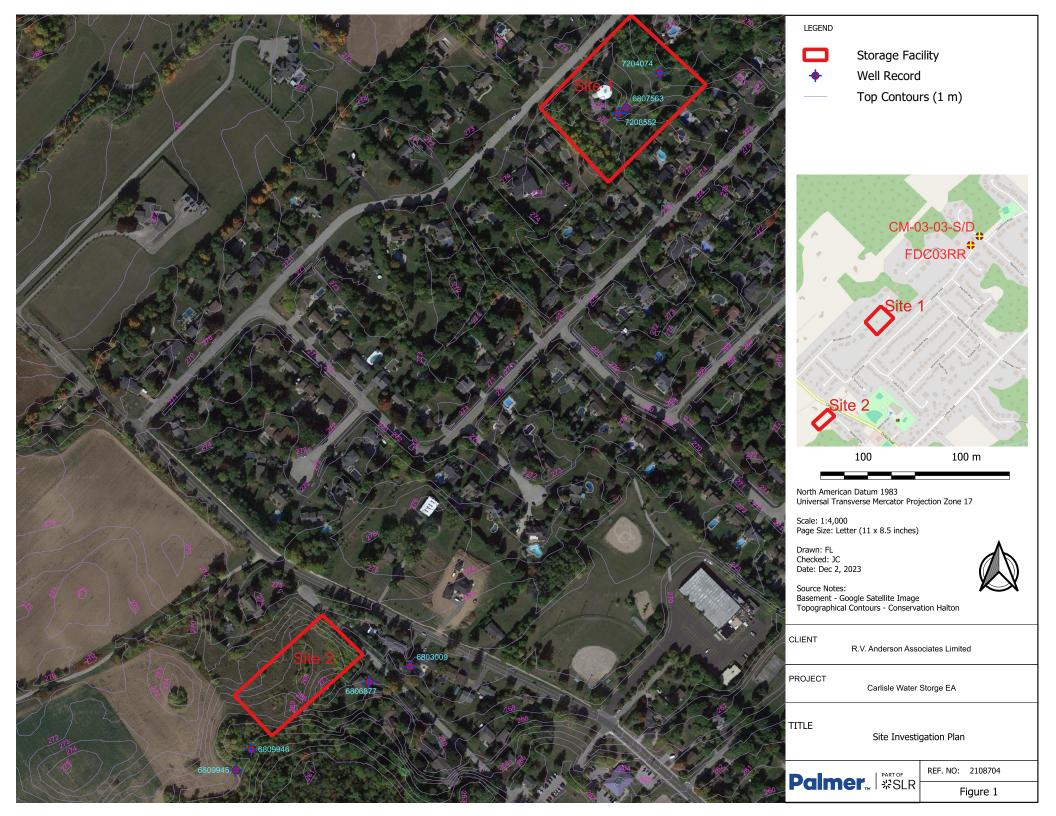


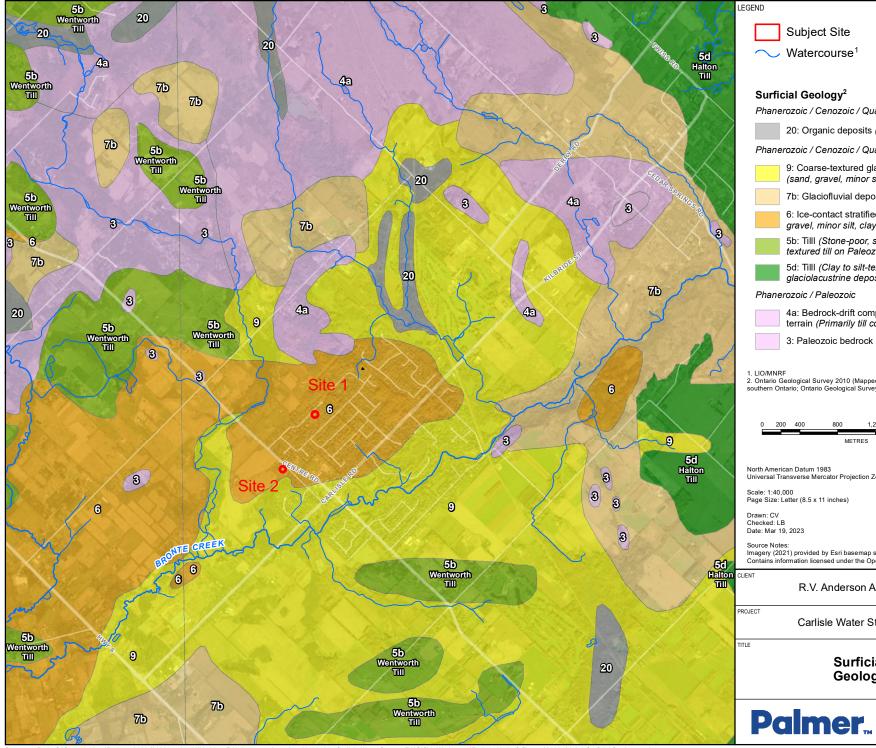
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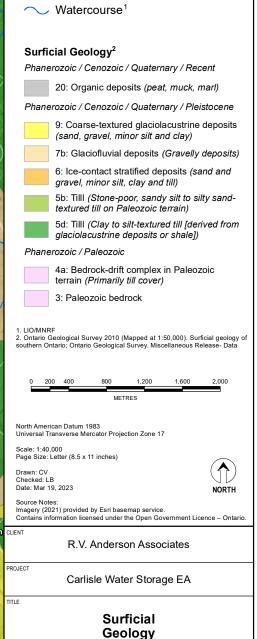
Attachment: Figure 1. Site Investigation Plan Figure 2. Surficial Geology Figure 3. Source Water Protection Appendix A: Well Records and Well Logs









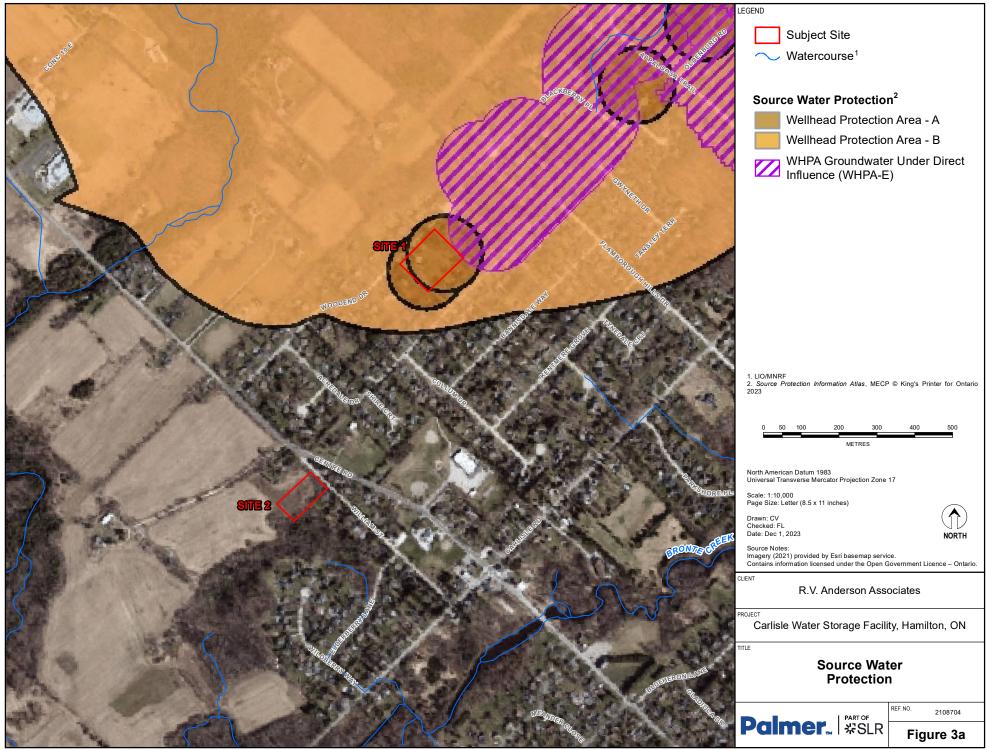


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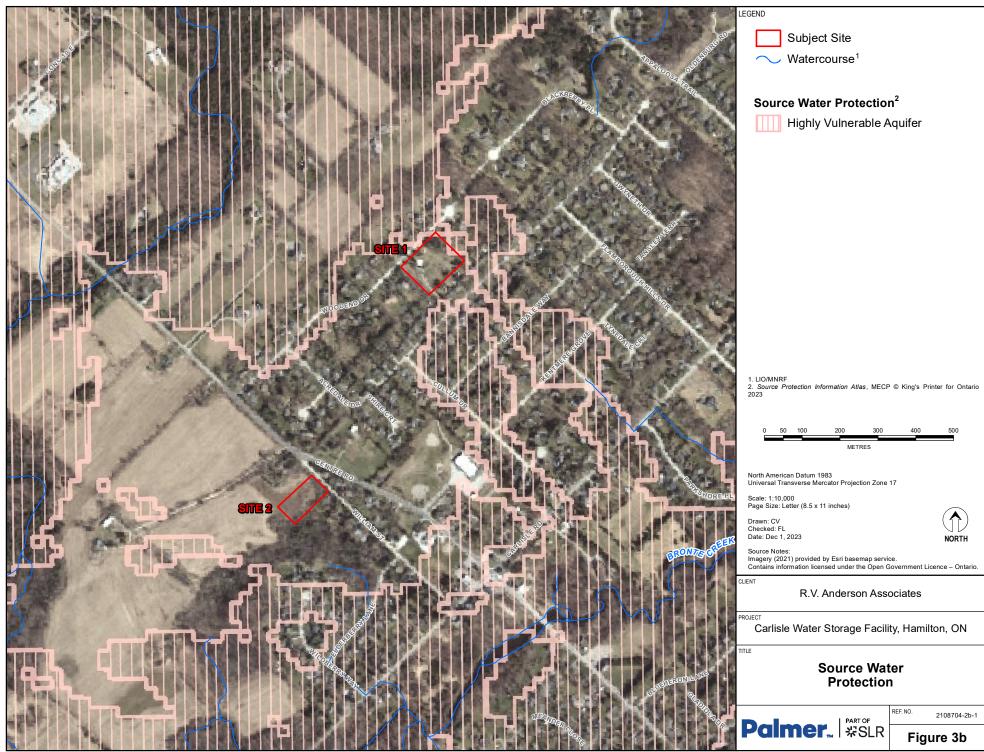
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Figure 2

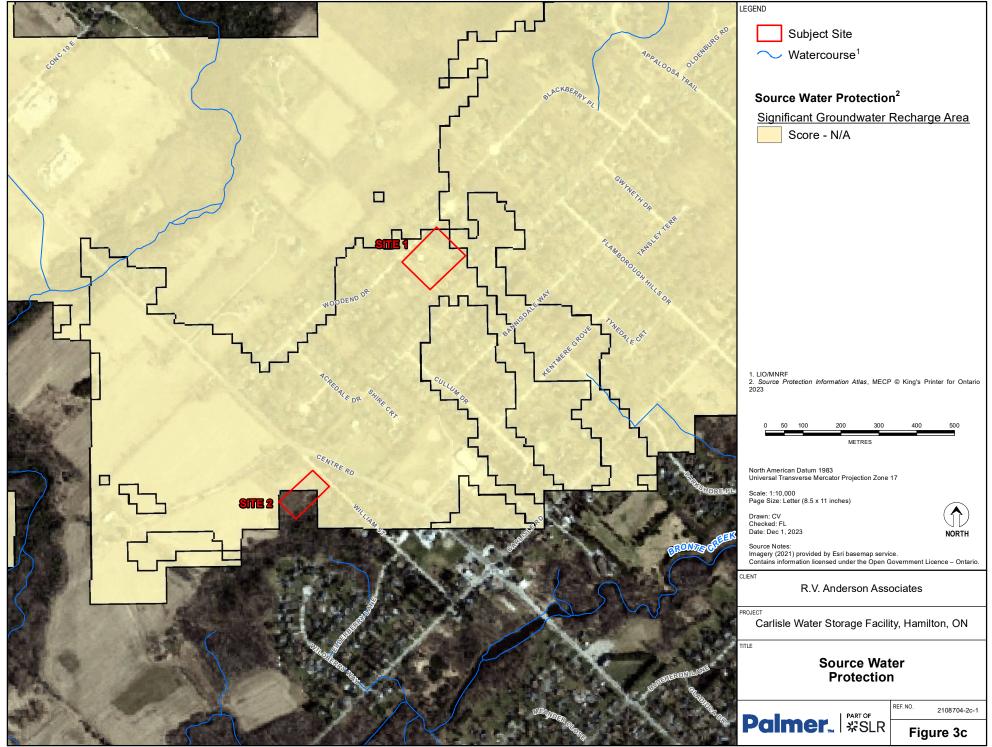
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MECP Water Well Records

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Ministry of the Environment

Well	Taq	No.
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Tag#: A131355

Regulation 903	Ontario Water	Resources A
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Measurem	nents recorded in:	🗌 Metric 🕠	Imperial	A1313	55 72085 5	52	Ū		Page		of
PLOYADINA SPERIO DALIGASI PARIS	ner's Informatio										
First Name	9 OF HAMILTON	Last Name	Organization			E-mail Address					Constructed ell Owner
	Idress (Street Numbe	er/Name)		N	lunicipality	Province	Postal Code		Telephone N		area code)
120 KIN Well Loc	NG ST. W.				HAMILTON	ONT	<u> 48P4V2</u>		905546	24241	
Address of	f Well Location (Stre	et Number/Name	e)	1	ownship		Lot		Concession		
	ALE DR. strict/Municipality				EAST FLAMBOROUG	H	06	Provin	09	Postal	Code
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	dinates Zone Eastir	-	Northing		lunicipal Plan and Suble	ot Number		Other			(rate, canada araa
		2407	4805895	- la durante and and	rd (see instructions on the	back of this form)					
General C		Common Materia			er Materials	[ral Description			Dep From	th (<i>m/ft)</i> ∣ To
						PACK AND SEAL EX	ISTING BED	ROCK			
						OVERDRILL EXISTI	NG 6" CASIN	G	0		41
						REMOVE PACK & S	EAL THEN FL	USH			
						BEDROCK			41		128
						HEAVY DUTY DRIV	E SHOE INST	ALL			
						ON END OF CASING	nd. nd				
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Denth S	et at (<i>m/ft</i>)		alant Used		Volume Placed	After test of well yield, v	Results of We water was:	the second s	d Testing aw Down	R	ecovery
From	То	(Material a			(m ³ /ft ³)	Clear and sand fr		Time (min)	Water Level (m/ft)	Time (min)	Water Level
6	41 NEET C	EMENT		400	GA	If pumping discontinue	d, give reason:	Static	41	(11111)	(nong
								Level	43.27	1	41.89
					· -	Pump intake set at (n	1/ft)	2	43.30	2	41.83
						70	an an an An Anna an Anna Anna Anna Anna An Anna Anna	3	43.30	3	41.76
Contraction of the second second	hod of Constructi			Well Use		Pumping rate (I/min / 0	GPM)				· · · · · · · · · · · · · · · · · · ·
Cable To	ool Dia Conventional) Dia	amond GP ting D		Commer Municipa		168US Duration of pumping		4	43.33	4	41.76
Boring	Reverse) 🗌 Dri			Test Hole		hrs + m Final water level end of		5	43.34	5	41.73
Air percu	ussion	In	dustrial			43.73	r parriping (mm)	10	43.40	10	41.63
Other, s	,	on Record - Ca	ther, specify		Status of Well	If flowing give rate (I/n	nin / GPM)	15	43.40	15	
Inside	Open Hole OR Mate	erial Wall	Depth	(<i>m/ft</i>)	Water Supply	Recommended pump	depth (m/ft)	20	43.43	20	
Diameter (cm/in)	(Galvanized, Fibregl Concrete, Plastic, St	ass, Thickness eel) <i>(cm/in)</i>	From	То	Replacement Well Test Hole			25		25	
6.2	STEEL	.219	+3	41	Recharge Well	Recommended pump (<i>l/min / GPM</i>)	rate	30	43.43	-30	
					Dewatering Well Observation and/or	168 Well production (I/min	/ GPM)	40	43.43	40	
					Monitoring Hole	Disinfected?		50	43.43	50	
					AConstruction) ☐ Abandoned,	Yes No		.60	43.47	60	
	Constructi	on Record - Scr	een		Insufficient Supply		Map of We				
Outside Diameter	Material (Plastic, Galvanized, S	Steel) Slot No.	Depth From	` ´	Water Quality	Please provide a map t ΛN	celow following i	nstructio	ons on the ba	ick.	
(cm/in)				То	specify		N				
					Other, specify	Nº,	//				
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Water foun	id at Depth Kind of \	r Details Nater: Fresh	Untested	and the second	(<i>m/ft</i>) Diameter	WE WARN					10.
	n/ft) ☐ Gas ☐ Other			From	To (cm/in)	¥/``	Ø	C	r. /	K.	00-
	id at Depth Kind of \ n/ft) □Gas □Othei			0	41 13			266	r. Dr	FD	
Water foun	d at Depth Kind of \	Vater: Fresh	Untested -			\sim		, V	AN OF		
(m	n/ft) ☐ Gas ☐ Other						Ì	//	KO10		
Business Na	Well Contr ame of Well Contract	actor and Well or	Technician		on Contractor's Licence No.			\mathcal{N}			
	opper and Sons Ltd			26					//		
	ddress (Street Numbe	er/ivame)			icipality	Comments:	-				
Province	32 Harpurhey Rd. Postal Cod	e Busines	s E-mail Addre		aforth	WELL# FDC01,PUM FROM TOC.			HOPPER,	MEAS	JRED
Ont-	NOK1WO	Name of Well	per@toc.on.	00 let Namo	irst Name)	information	ckage Delivered		Ministr Audit No.	y Use	Only
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Well Technici	21737 an's Licence No. Sign	ature of Technicia	an and/or Con	tractor Date	Submitted		1 1				
2576 0506E (2007/1	2) © Queen's Printer fo	or Ontario, 2007	<u>~</u> ~	<u>- IYP</u>	2/08/2013/ D D Ministry's Copy	<u>, ∟ №</u> , data Y 017	08/2013		OCT 0	1 20	113

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307/50 on IX JB. UTM 117 2 5821120 CODED DIVISION OF 6806877 WATER RESOURCES 141R 14181015 710 N JAN 9 1969 Ontario Water Resources Commission Act Elav. ONTARIO WATER RECOR Basin RESOURCES COMMISSION County or .Township, Village, Town or City. 8 Con..... ...Lot. Date completed (dav Owne Address (print in block letters) a Casing and Screen Record **Pumping Test** Inside diameter of casing 29 Static level Total length of casing Test-pumping rate G.P.M. Type of screen Pumping level Length of screen Duration of test pumping /m Depth to top of screen. Water clear or cloudy at end of test 6' Diameter of finished hole Recommended pumping rate. G.P.M. with pump setting of 60feet below ground surface Well Log Water Record Depth(s) at Kind of water Overburden and Bedrock Record From To ft. which water(s) (fresh, salty, sulphur) ft. found 35 35 60 61 For what purperers) is the water to be used?... Location of Well asl frulloge 1 boulish In diagram below show distances of well from road and lot line. Indicate horth by arrow. Is well on upland, in valley, or on hillside LOT Drilling or Boring Firm مرجم PK20 Address. WV 1) Licence Number Name of Driller or Borer Ĵ Address Date / (Signature of Licensed Drilling or Boring Sontractor) whow ocross the Form 7 OWRC COPY Kood CSS.S8

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	Brown		Clay	Sand	Stor										10	20
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					Grav	rels									52	55
	Brown	1	Clay	Sand	Grav	rels			••••						55	60
	Gray		Rock				·								60	70
).[Gray		Rock												70	87
	Blue		Shale	38											87	96
	Red		Shale	8											96	100
	STAT LEVI -DE Flow IF FLOWIN GIVE RATE	2 5 2 5 3 1 2 5 3 1 2 5 3 1 2 5 3 1 4 2 5 1 7 2 3 1 6 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 8 1 19 1 19 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1 11 1 12 1 13 1 14 1 15 1 16 1 17 1 18 1	SALTY 4 IRESH 3 SALTY 4 IRESH 3 IRESH 3	MINERAL SULPHUR ¹⁹ MINERAL SULPHUR ²⁴ MINERAL SULPHUR ²³ MINERAL SULPHUR ³⁴ O PUMPING RATE ²⁵ WATER LI ⁴ ¹ PUMP INTAKE S N RECOMMENDED PUMP	0811 17-18 0811 24-25 24-25 040 cevels durin 30 minute 2 r tet at	G 45 M 9-31 EET WATER J	12 12 12 12 14 15 15 16 15 16 16 15 16 16 17 17 16 17 17 17 17 17 17 17 17 17 17	OO JIMPING COVERY OO DO TEST 2 CLOU	62 17-18 MINS 535-37 Weet 42	20-23 0100 27-30	GRAM BELC	SET AT - FEET TO -13 14 -21 22- -29 30- O C AT I O OW SHOW DIS DICATE NORTH	GGING MA 225 23 80 0 N O F STANCES	& SEALII TERIAL AND T WELL OF WELL FF	YPE ICEMI LEAD P	ENT GROUT ACKER. ETC)
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CONTRACTOR		DRILLER C	ins 2			SUBMISSION D	ATE								CSS.S	- QU

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Min of th	istry he	VAT				RD
Ontario	rironment	spaces provided	68099		(0)	109
COUNTY OR DISTRICT	2. CHECK 🗵 COR	TOWNSHIP, BOROUGH, CITY, TOWN, VILLAGE	00000	CON., BLOCK, TRACT, SURVEY		008,
Montword	th Hamilton	F Plemboro	REC.C.	9 IERED ONT	DATE COMPLETED 05	48-53
		isle, Ontar	10 #	386392	DAY 24 MO	у _{ук.} <u>79</u>
	м 10 т2			RC. BASIN CODE		
	L	OG OF OVERBURDEN AND BEDRO	OCK MATERIA	S (SEE INSTRUCTIONS)		
GENERAL COLOUR	MOST COMMON MATERIAL	OTHER MATERIALS		GENERAL DESCRIPTION	FROM	TH - FEET
	Top soil				0	1
Brown	Clay	Stones			1	10
Brown	Clay Sand	Stones			10	20
Brown	Clay Sand	Gravels			20 40	40 Z
Brown	Clay Sand	Gravels			60	73
Br. Gray	Rock				73	87
. Gray Blue	Shales				87	95
Red	Shales				95	100
		T.W. 2				
31 000	02 001	060512 00206052812	0060605	2811 007361278	09872121	<u>69</u> []
				54 SIZELSI OF OPENING 3	65 1-33 DIAMETER 34-38	75 BO
41 WA WATER FOUND AT - FEET	ATER RECORD	CASING & OPEN HOLE	DEPTH - FEET	C ISLOT NOT	INCHES	
10-13 1	FRESH ³ ☐ SULPHUR □ SALTY ⁴ □ MINERAL	DIAM. MATERIAL THICKNESS F INCHES INCHES F	ROM TO 13-16	MATERIAL AND TYPE	DEPTH TO TO OF SCREEN	IP 41-44 30 FEET
15-18 1	FRESH ³ ULPHUR ¹⁹	2 GALVANIZED 3 □ CONCRETE 4 □ OPEN HOLE -250 (0 00 61	61 PLUGGING	& SEALING REC	CORD
	□ SALTY ⁴ □ MINERAL □ FRESH ³ □ SULPHUR ²⁴	4 □ OPEN HOLE 6 & 20 0 17-18 1 □ STEEL 19 3 □ GALVANIZED	20-23	DEPTH SET AT - FEET M		EMENT GROUT D PACKER ETC)
2	$\square SALTY \stackrel{4}{\square} MINERAL$ $\square FRESH \stackrel{3}{\square} SULPHUR \stackrel{29}{\square}$	087 3 CONCRETE	51 (0100	10-13 14-17		
	□ SALTY 4 [] MINERAL	24-25 1 STEEL 26 2 GALVANIZED 3 CONCRETE	27-30	18-21 22-25 26-29 30-33 80		
2	SALTY 4 MINERAL	COPEN HOLE				
71 PUMPING TEST M		11-14 DURATION OF PUMPING 0040 GPN 24 15-16 00 17-18 HOURS 00 MINS		LOCATION O	FWELL	
STATIC LEVEL	WATER LEVEL 25	LEVELS DURING 2 M RECOVERY	IN DIA LOT L	GRAM BELOW SHOW DISTANCES INE. INDICATE NORTH BY ARE		AND N.
	21 22-24 15 MINUTE 26	S 30 MINUTES 45 MINUTES 60 MINUTES 5-24 29-31 32-34 00 35-37			Å	71
S IF FLOWING, GIVE RATE	ET 004 FEET F 38-41 PUMP INTAK	FEET FEET FEET FEET FEET FEET FEET FEET	Con Lets	9		
	OOOL GPM	FEET 1 X CLEAR 2 CLOUDY VED 43-45 RECOMMENDED 46-49	LOTS	84 600- >1		
SHALLO	DW DEEP SETTING	040 FEET RATE 0040 GPM		× 1		
	54 1 WATER SUPPLY	5 🗍 ABANDONED, INSUFFICIENT SUPPLY	1			
FINAL STATUS	2 DOBSERVATION W			1500	. 1145 °	
OF WELL	4 RECHARGE WELL 55-56 1 DOMESTIC	5 🙇 COMMERCIAL			Votaliste	e
WATER	2 STOCK 3 I IRRIGATION	MUNICIPAL PUBLIC SUPPLY		<u> </u>		
USE (COOLING OR AIR CONDITIONING P NOT USED				
METHOD	57 1 🗶 CABLE TOOL 2 🗌 ROTARY (CONVE		11 -	BRONTE CREE		
OF	→ □ ROTARY (REVER: → □ ROTARY (AIR)	SE) Ø 🗍 JETTING 9 🗋 DRIVING		Unite		
L	S AIR PERCUSSION	LICENCE NUMBER	DRILLERS REMAR			7 6 3-6a 80
🖉 Graha	m Well Drill				0.1.06	
ADDRESS	h, Ontario	_	SE	CTION INSPECTOR	11/0	24/87
NAME OF DRIL	LLER OR BORER	LICENCE NUMBER				/
SIGNATURE OF		SUBMISSION DATE	OFFICE		088.00	
MINISTR	Y OF THE ENVI	RONMENT COPY			FORM	M NO. 0506-477
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Basin	ria Water Re	sources Comm	inion Ast 105		Ì.
F \$:= 1				ONTARIO WATER	SION
WAT	ER W	ELL I	RECOR	D	
County or District Wintworth		Township,	Village, Town or	r City & F	loniboro
Con 9 Lot 7			pleted	may	59
		ress	6 orlis	6 P.O.	year)
Casing and Screen Record				mping Test	
Inside diameter of casing		Static lex		7	
Total length of casing 568			ping rate	20	G.P.M.
Type of screen Monde			level 4		
Length of screen			of test pumping	-	
Diameter of finished hole			ear or cloudy at ended pumping	end of test	2
	ĩ		pumping level of	. .	G.P.M.
Well Log				ter Record	
	From	То	Depth(s) at which		Kind of water
Overburden and Bedrock Record	ft.	ft.	water(s) found	No. of feet water rises	(fresh, salty, sulphur)
Sonly loon	0	35	71	211	hat
- little little	35				- Avon
- oury worm		65			
for	65	#67			
Rak	\$\$67	72			
	-				
For what purpose(s) is the water to be used?		M	Locati	on of Well	Ar
house	2			how distances of	well from
Is well on upland, in valley, or on hillside?	hillsife	1 11		Indicate north	
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Form 5 15M-58-4149		}	CACK AN		C\$\$.\$*

Palmer.

Well Log FDC03RR

Method: Cased rotary-percussion drilling

Diameter: 400 mm

REF. NO.: 2108704

PROJECT: Carlisle Redundant Well

CLIENT: R.V. Anderson Associates Limited

PROJECT LOCATION: 84 Acredale Drive Carlisle, ON

DATUM: Geodetic

Date: Apr-17-2023 to Apr-20-2023 ENCL NO .: BH LOCATION: DYNAMIC CONE PENETRATION RESISTANCE PLOT SOIL PROFILE SAMPLES PLASTIC NATURAL MOISTURE IMIT CONTENT REMARKS GROUND WATER CONDITIONS LIQUID LIMIT AND LIMIT 40 POCKET PEN. (Cu) (kPa) 20 60 80 100 I (m) STRATA PLOT GRAIN SIZE Wp w W BLOWS 0.3 m NATURAL U SHEAR STRENGTH (kPa) O UNCONFINED + FIELD VANE QUICK TRIAXIAL × LAB VANE ELEVATION ELEV DEPTH DISTRIBUTION -0 _ DESCRIPTION NUMBER (%) WATER CONTENT (%) TYPE ż 20 40 60 80 10 20 30 100 273.0 Ground Surface GR SA SI CL **FILL:** sandy gravel to gravelly sand, trace clay, subrounded dolostone Bentonite Seal 0.0 272 and sandstone gravel (<30 mm), brown, wet to moist, no stain and no 1 GR odor. a few rootlets and anthropogenic debris. 270 269.2 2 GR SANDY GRAVEL TO GRAVELLY 3.8 ò SAND: trace clay, subrounded to 3 GR 268 subangular dolostone, limestone and sandstonegravel (10 to 35 mm), ۰o brown, damp to dry at top, no stain 4 GR 0 and no odor. 266 - clean water was used as drilling 0 fluid. 5 GR Cement Grout 0 6 GR V W. L. 262.5 m 261.9 7 GR SANDY GRAVEL: subrounded to May 01, 2023 11.1 subangular dolostone and precambrian rock gavel (<30 mm), 8 GR 260 greyish brown, no stain and no odor. 258.5 9 GR 14.5 DOLOSTONE: fine-crystallized, 258 slightly weathered at upper part, a 10 GR few vugs and solution holes, geyish white. 256 255.5 GR 11 LIMESTONE: fine-crystallized, 18 17.5 grey. 12 GR 254 ----fractures. 252.4 13 GR 20.6 LIMESTONE and DOLOSTONE: 252 interlayered limestone and 14 GR dolostone, fine-crystallized, Vuggy and fossiliferous locally, a few fractures, light grey. 250 15 GR --- fractures. 16 GR 248 Open Hole -- abundant vugs and fossils (25 to 17 GR 27 mbgs). 246 GR 18 244.1 244 **LIMESTONE:** fine-crystallized, thinly bedded, with siltstone 28.9 19 GR interlayers at lower part, grey. 20 GR 242 240 5 21 GR SHALE: calcareous shale with siltstone interlayers, greenish grey. 2**30.0** 33.0 22 GR END OF BOREHOLE Notes: Grab samples of cuttings were taken with fine mesh strainer. Loss of fine materials is anticipated. The well log was based on cutting classfication and records of construction

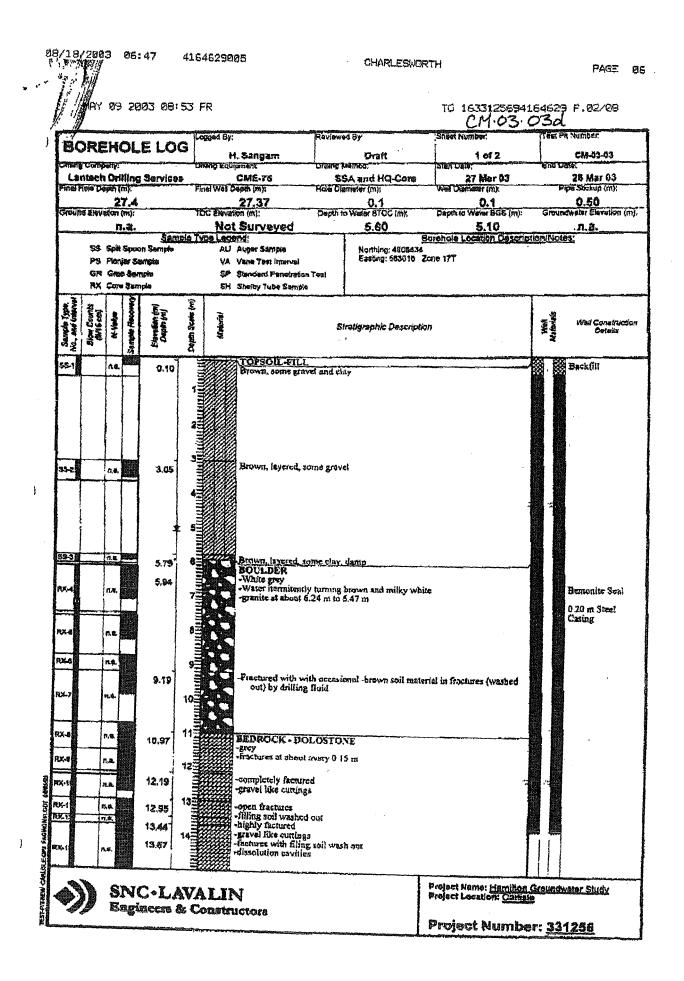
GROUNDWATER ELEVATIONS T

Deep/Dual Installation 🗴 🗴



+ ³, × ³: Numbers refer <u>GRAPH</u> NOTES to Sensitivity

O ^{8=3%} Strain at Failure



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TO 1633125694164629 P.03/06

Tost PR Number: Sheet Number) cogged By: Revenued By. BOREHOLE LOG CM-03-03 2012 H. Sangam Draft Borehole Lecition Description/Notes: Sample Type Legend; Northing: 4575434 Easting: 563016 Zone 17T SS Spill Spoon Sample ALS Auger Sample VA Vene Test interval PS Piorder Samples SP Standard Penetrepon Test GR Greb Sample SHI Sherry Tube Sample RX Core Sample Ē Brow Counts (115 cm) Etwation (m) Depth (m) Strack Type, No. and interv Wex Matherials Sarrida Necon Pi-Vision Material Diaph Scale Well Construction Stratigraphic Description Details -frectured, open fractures -shundant dissolution cavities 15.24 16 RX-1 机制 17 -bighly fractured sungular gravel like cuttings 17.22 18= RE # 17.10 193 -micropones -rough core 18.97 -highly factured -gravel like combass 19.76 20 0.10 m Diameter PX-19,**8** Open Hole from 13.72 mbgs to 27.37 mbgs 21Ξ -micropores -rough core surface 21.13 FOL ! ... 22= -Intact rock, no factures 22.60 ET. 23 ñ.s. -mooth one surface R.K.-1 74 E SHALE 24.33 -dark grey, very stiff -plasho clay seams starting at about 25.5 mbgs -clay seams at every 0.1 to 0.20 m -becoming greenish with depth 25 83.2 n.4 263 2.2 4 27 End of Borchole 27.37 504 Notional Party of the 3 Project Name: <u>Hemilton Groundwater Study</u> Project Location <u>Carlinia</u> SNC-LAVALIN Engineers & Constructors Project Number: <u>331256</u>